

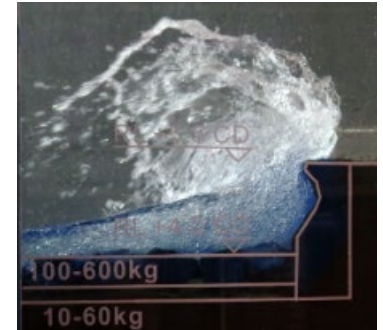
Wave overtopping mitigation by a vertical wall or a wave return wall at the end of a pitched rock slope

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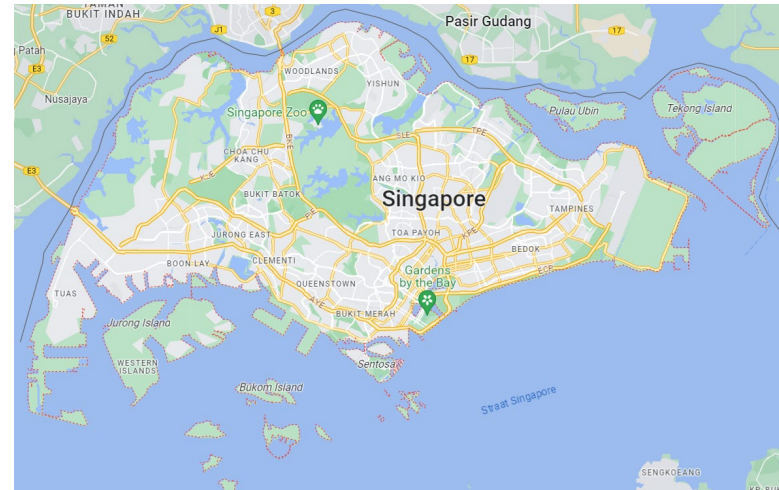
- Objective
- Mitigation options for sea level rise and wave overtopping
- Stability of pitched rock slopes
- Analysis on wave overtopping
- Practical results along EurOtop

Situation in Singapore

- Relatively mild (design) wave conditions: $H_s = 1-2.5$ m
- Locally generated: steep waves with $s_{m-1,0} > 0.035$
- Deep water (generally 10-20 m)
- Crest level low and equal to industrial area

Sea level rise will have a significant influence on wave overtopping

What are efficient and practical mitigation options?



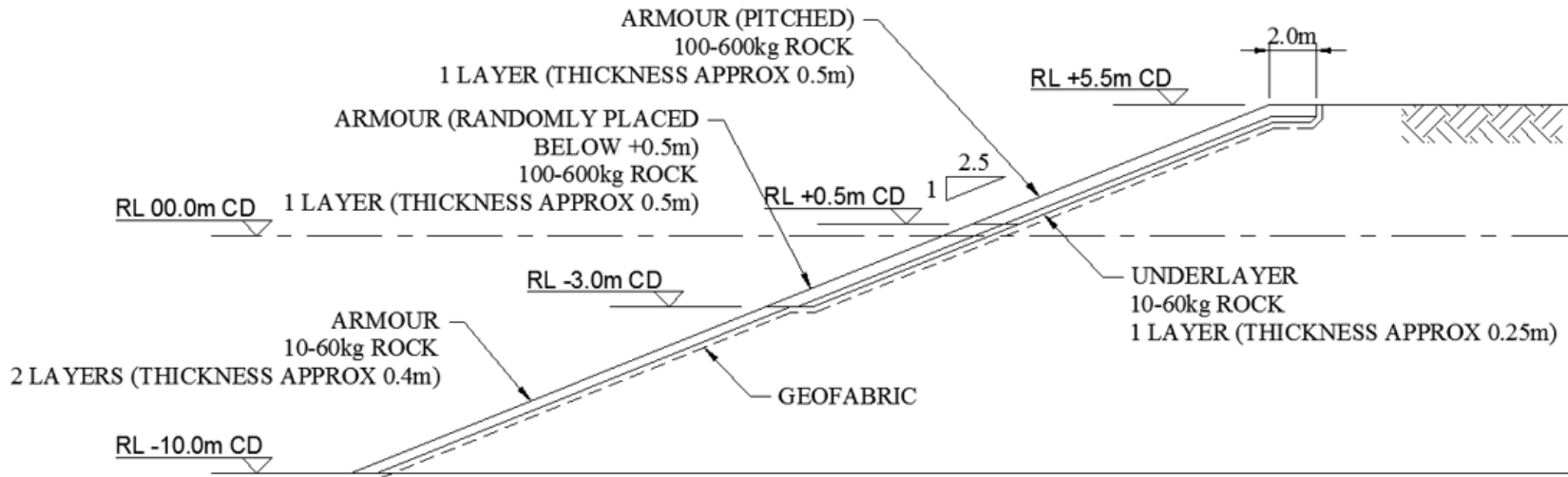
Pitched rock slopes



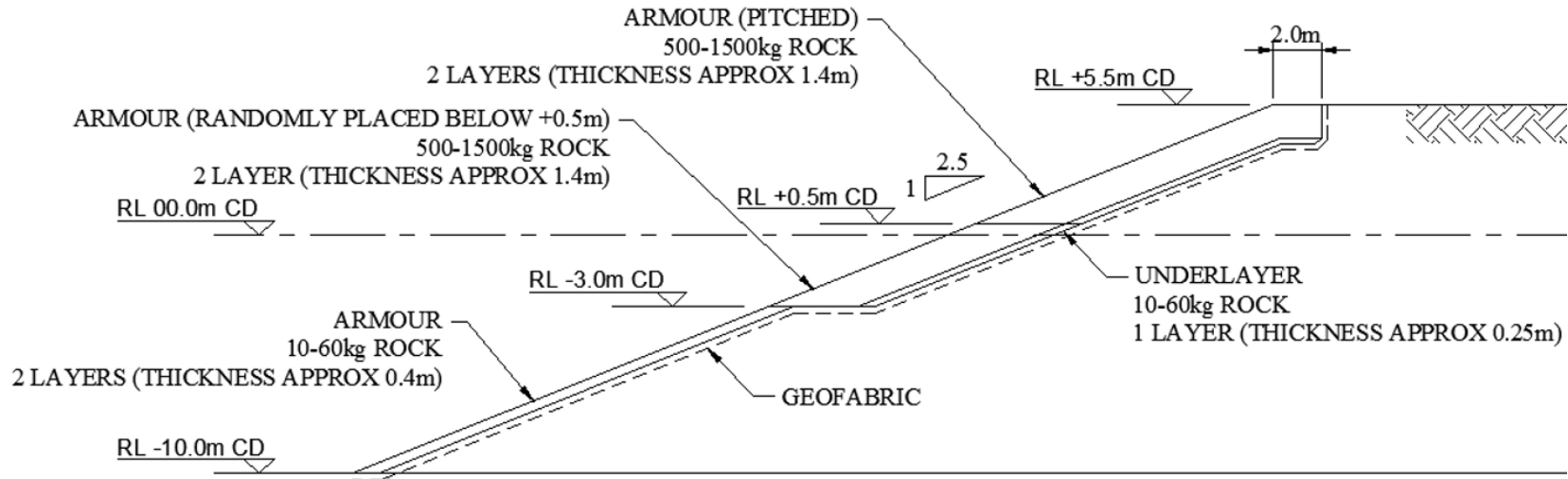
Pitched rock slopes



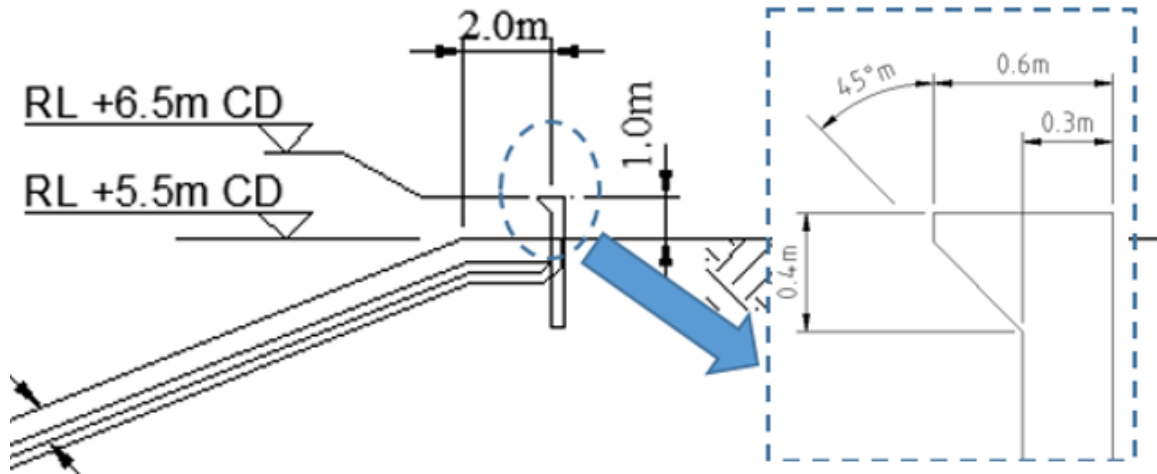
Pitched rock slopes – single layer, Structure 1



Pitched rock slopes – double layer, Structure 2



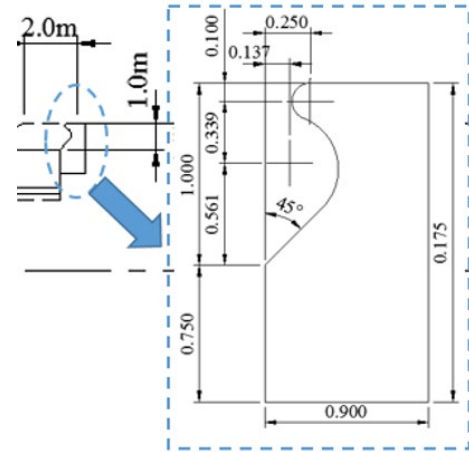
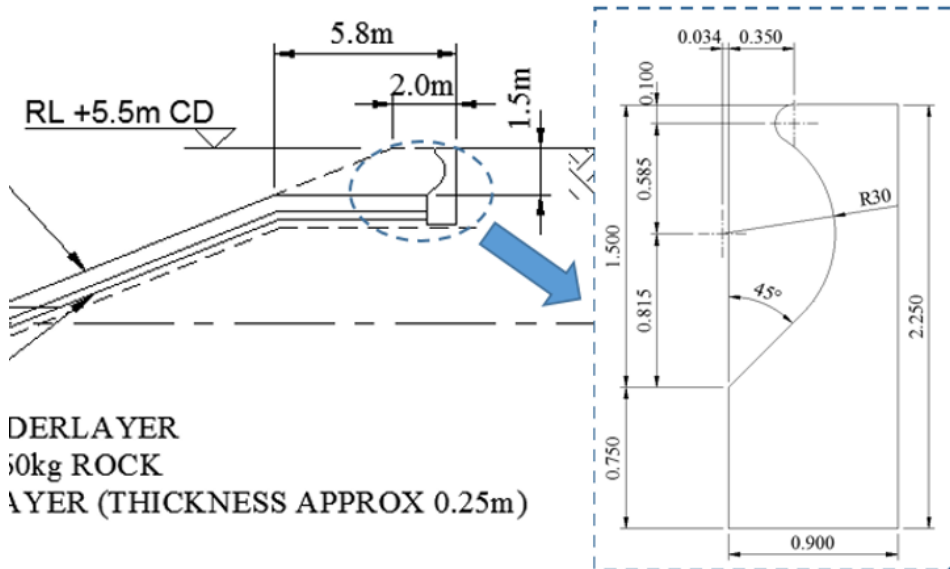
Mitigation: wave wall



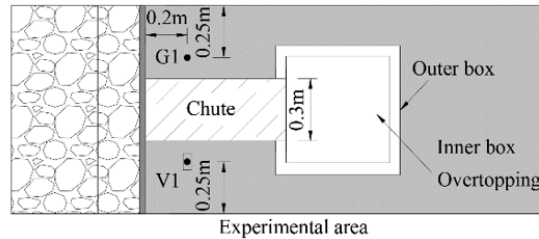
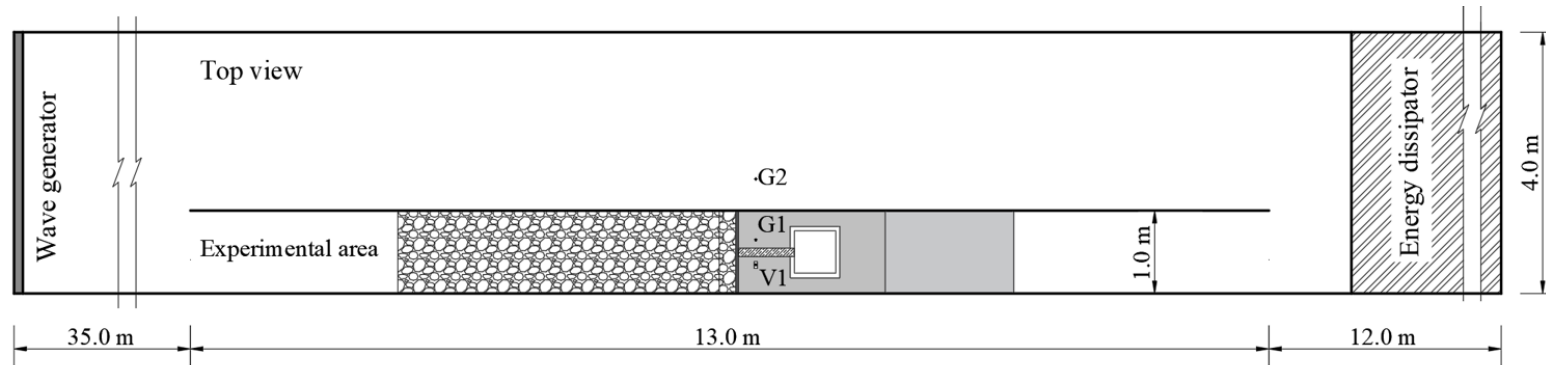
1.0 or 1.5 m high
with or without bullnose

Mitigation: wave return wall

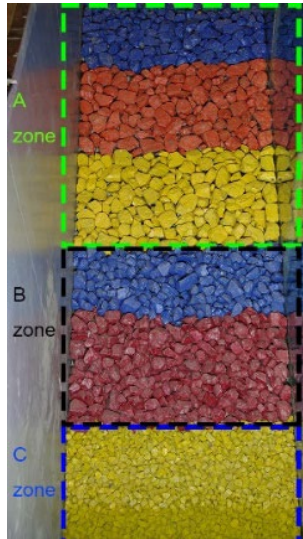
1.0 or 1.5 m high



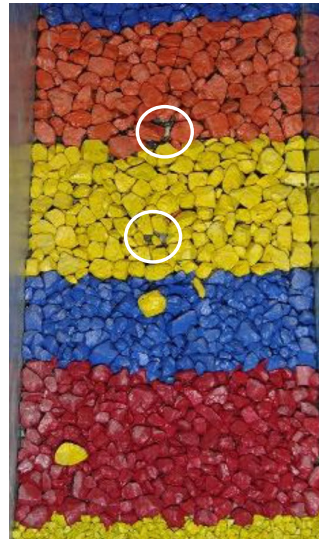
Model tests in China, Dalian University of Technology



Single layer



Before



$S_d = 1.2$

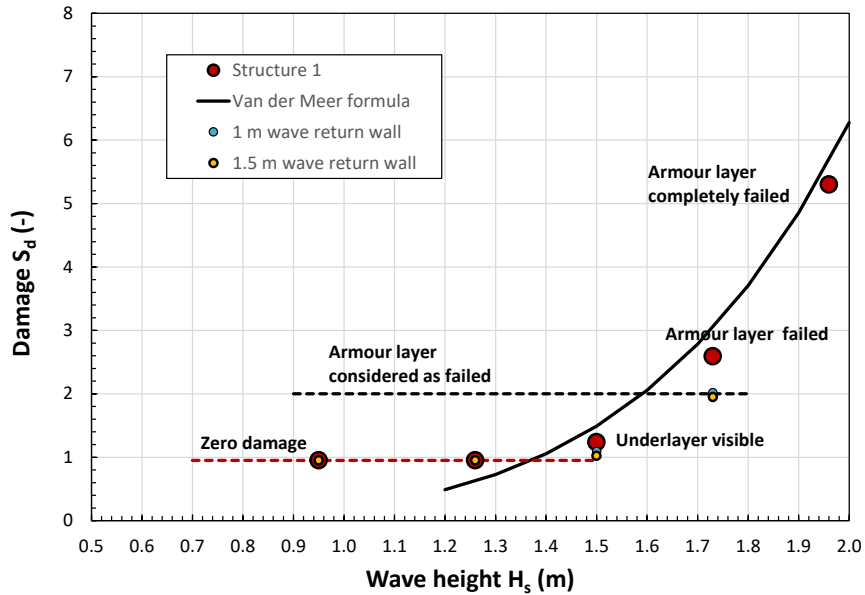


$S_d = 2.3$
Failure

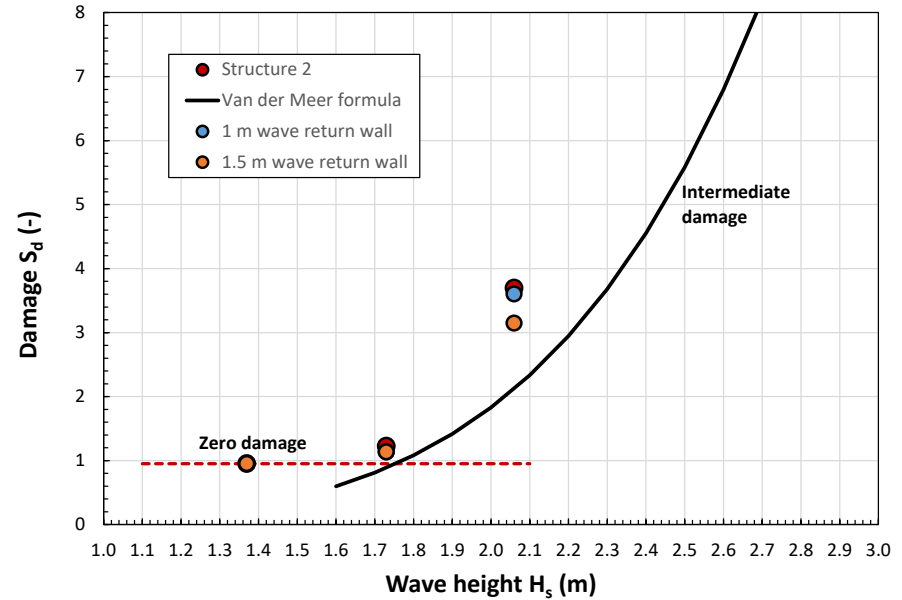


$S_d = 4.6$
Structure failed

Stability – Van der Meer formula



Single layer pitched rock



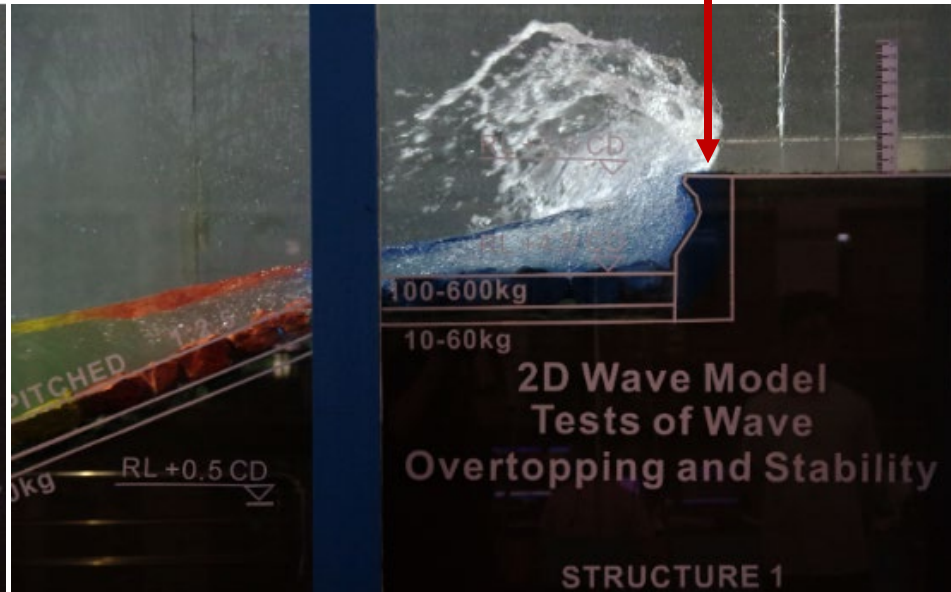
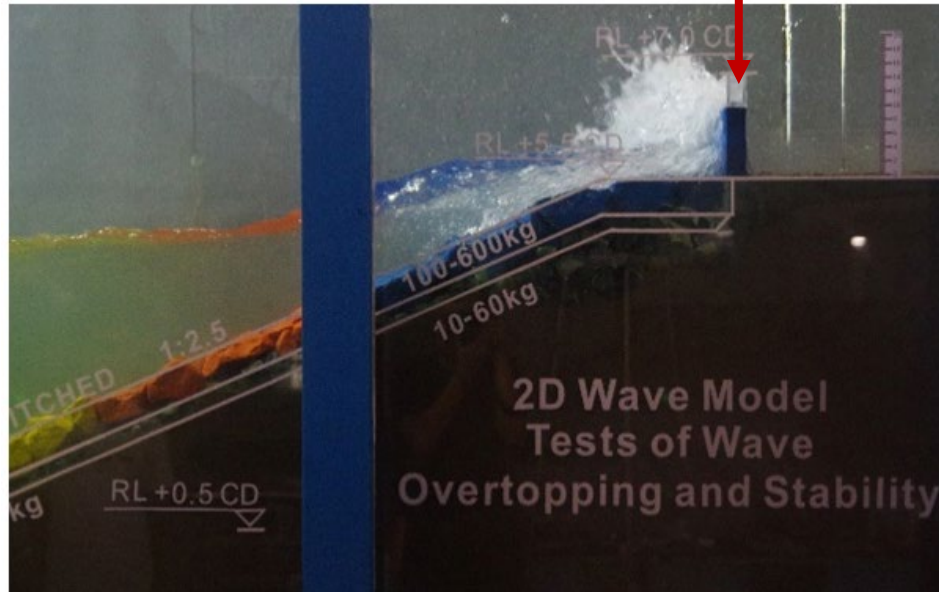
Double layer pitched rock

Wave overtopping tests

Wave wall, with or without bullnose



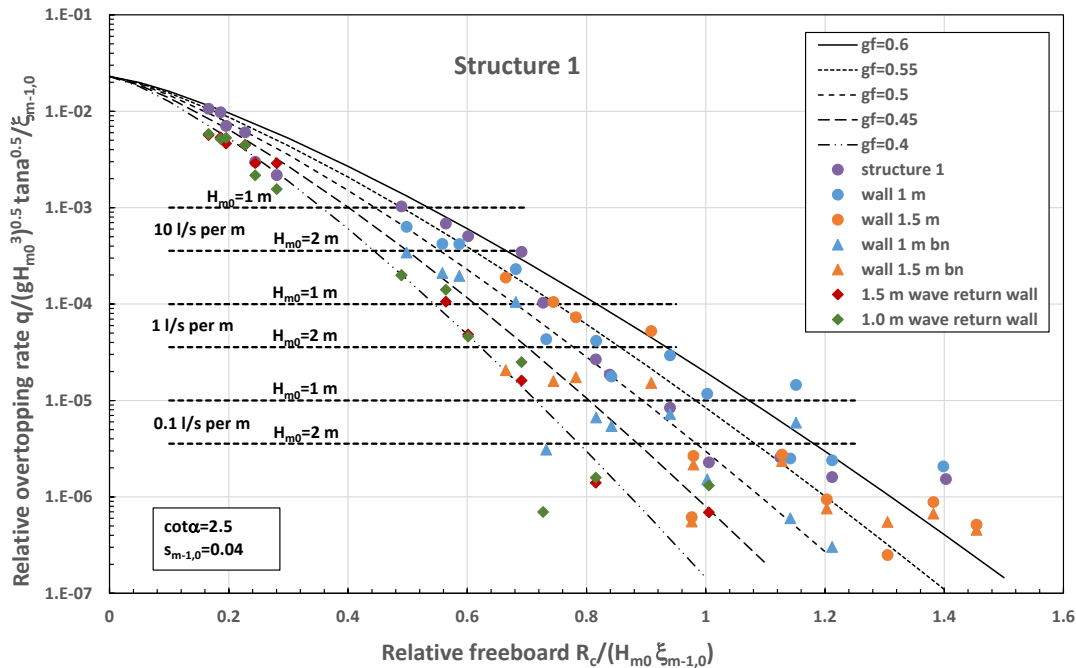
Wave return wall



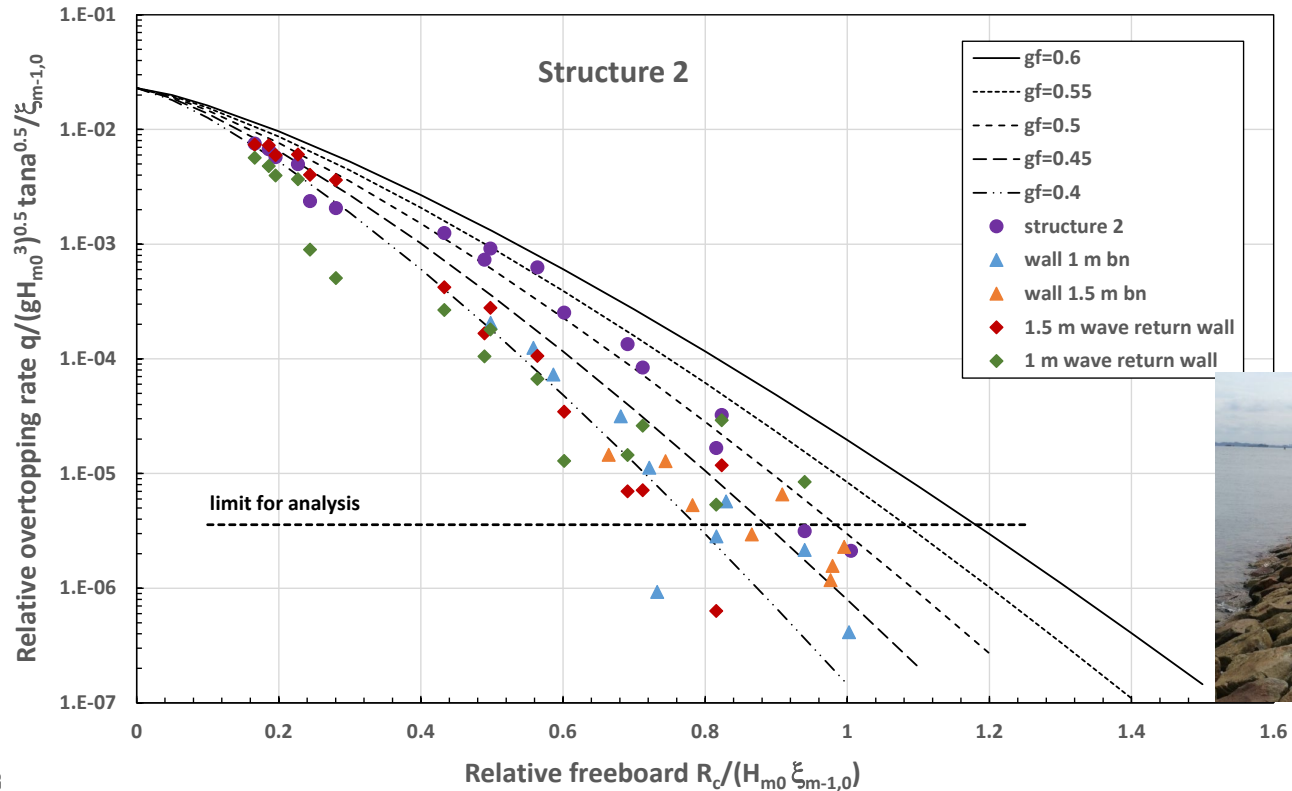
EurOtop equations (gentle slope)

$$\frac{q}{\sqrt{g \cdot H_{m0}^3}} = \frac{0.023}{\sqrt{\tan \alpha}} \gamma_b \cdot \xi_{m-1,0} \cdot \exp\left[-\left(2.7 \frac{R_c}{\xi_{m-1,0} \cdot H_{m0} \cdot \gamma_b \cdot \gamma_f \cdot \gamma_\beta \cdot \gamma_v}\right)^{1.3}\right]$$

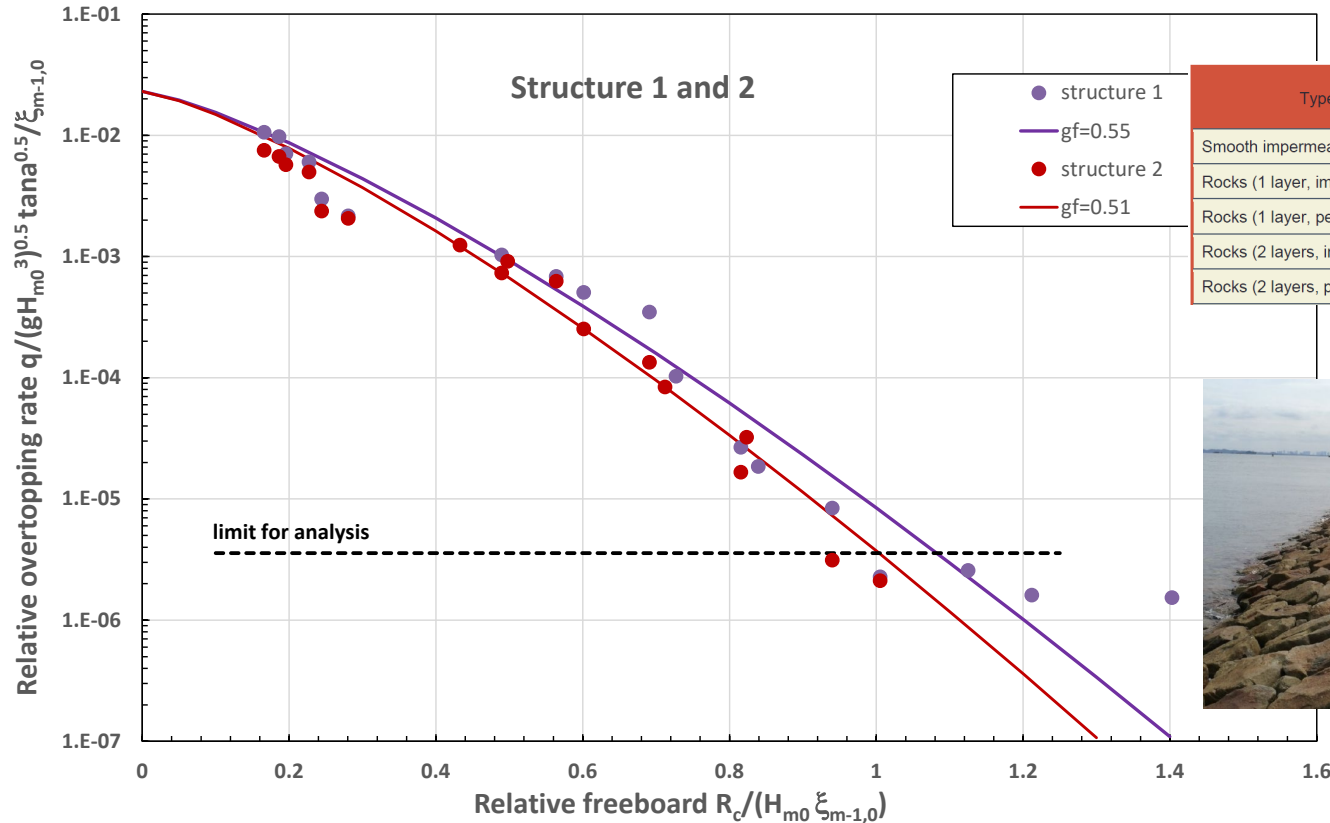
Influence factor for roughness/wall
EurOtop 5.10



Double pitched, all data



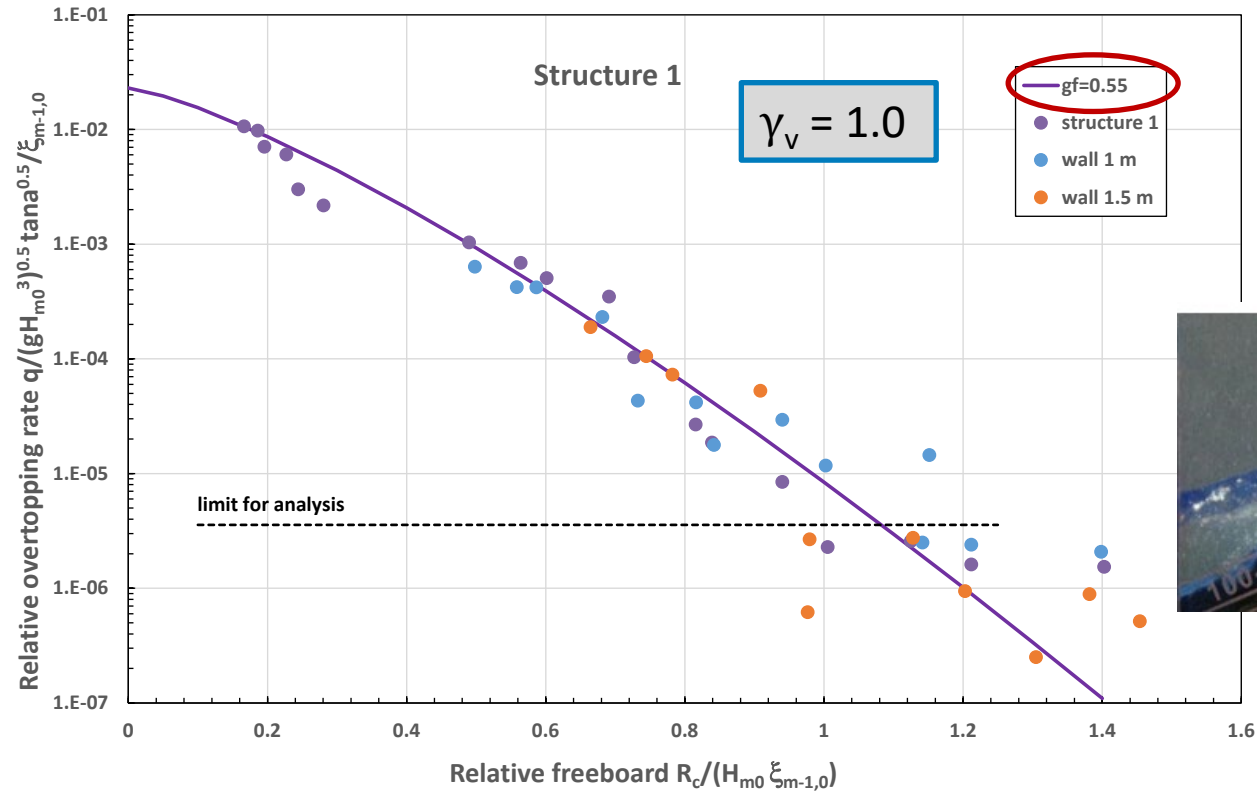
Single or double pitched - comparison



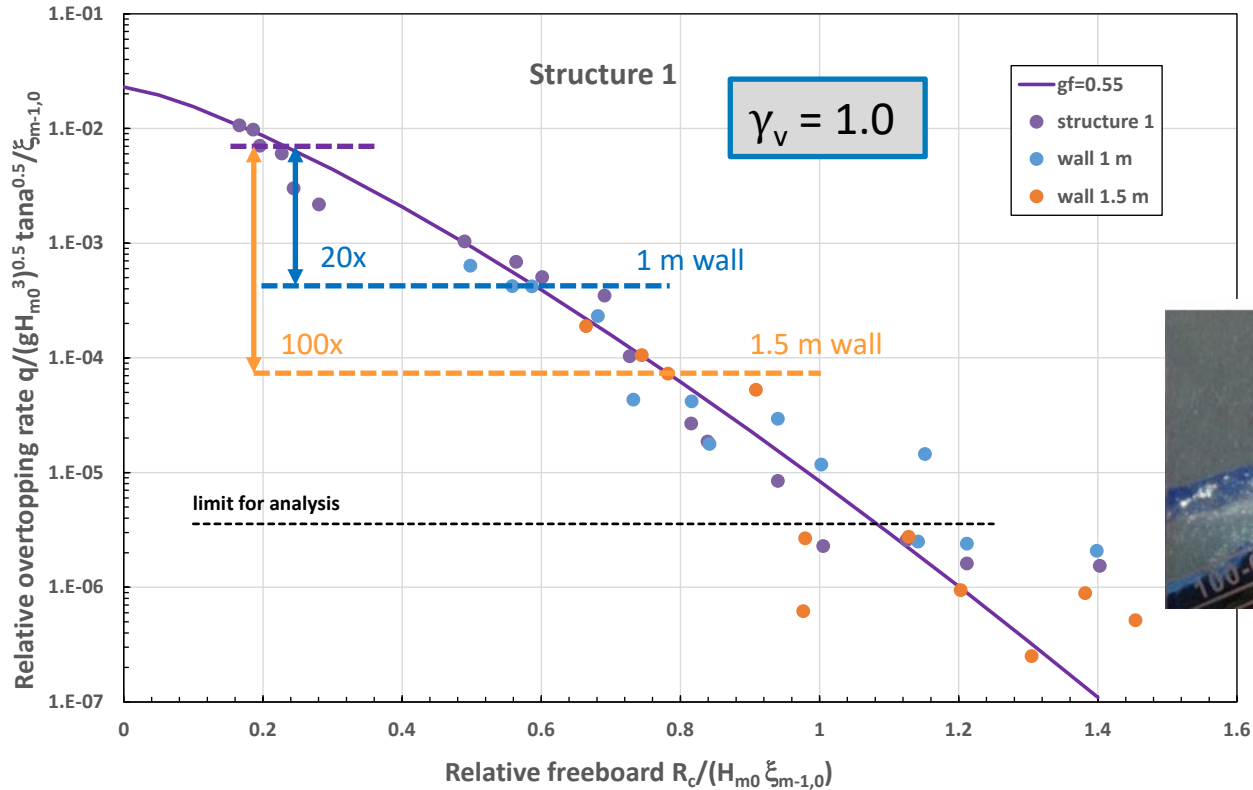
Type of armour layer	γ_r
Smooth impermeable surface	1.00
Rocks (1 layer, impermeable core)	0.60
Rocks (1 layer, permeable core)	0.45
Rocks (2 layers, impermeable core)	0.55
Rocks (2 layers, permeable core)	0.40



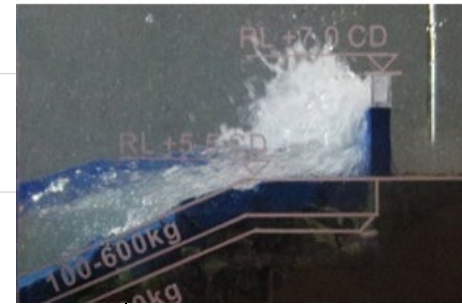
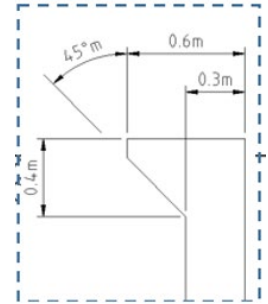
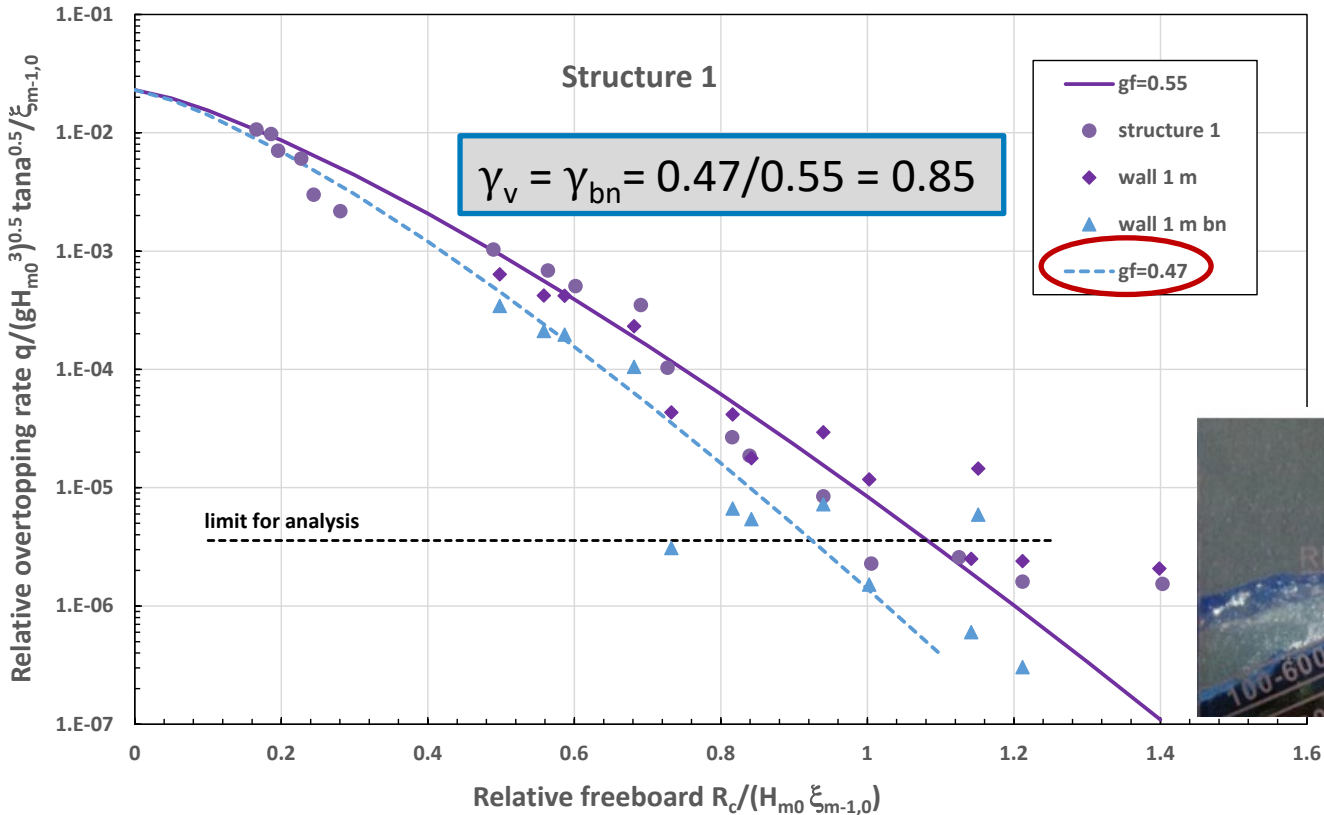
Single pitched; wave wall



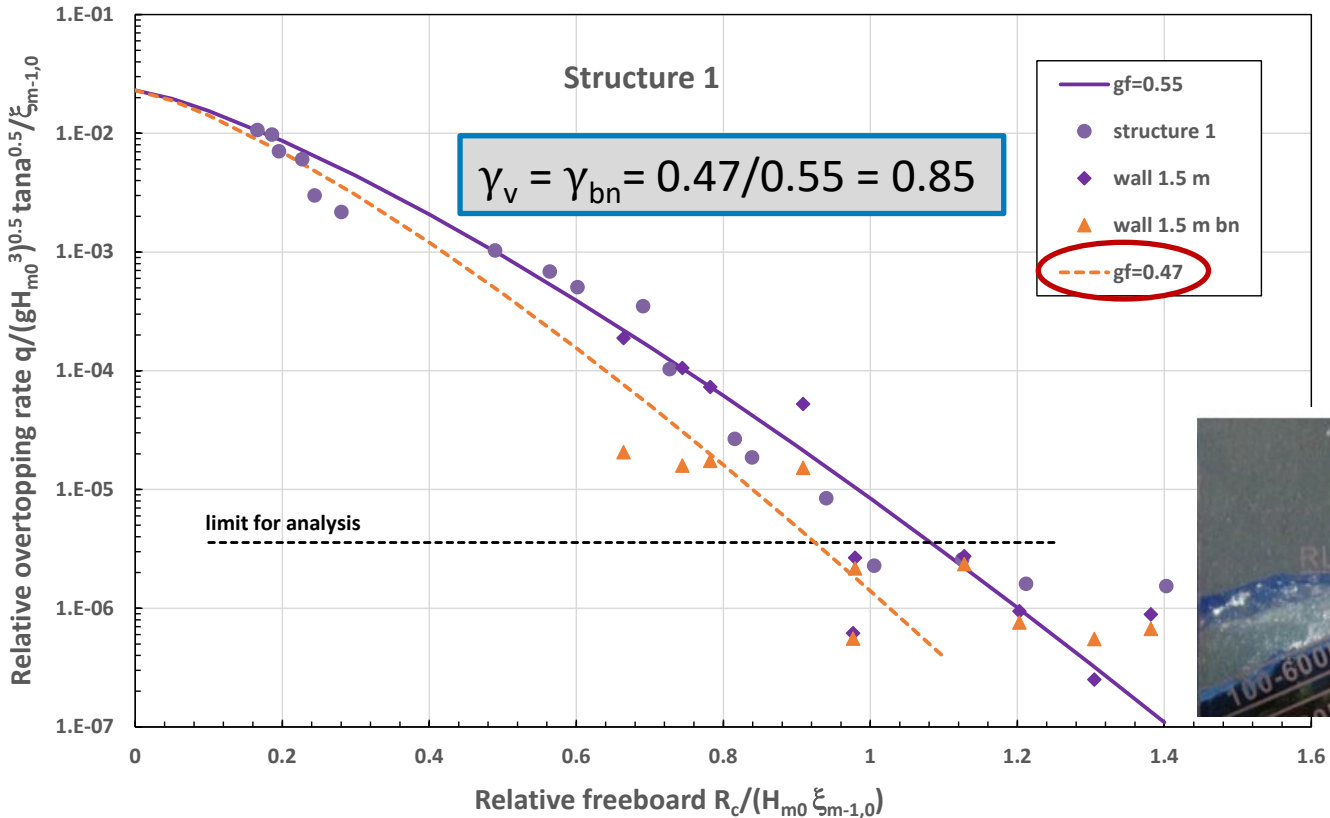
Single pitched; wave wall



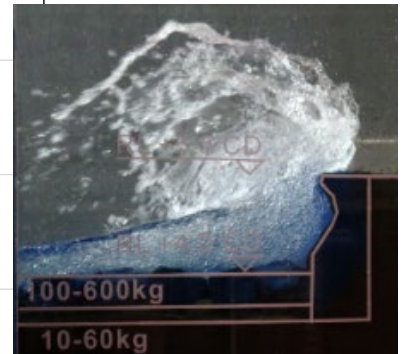
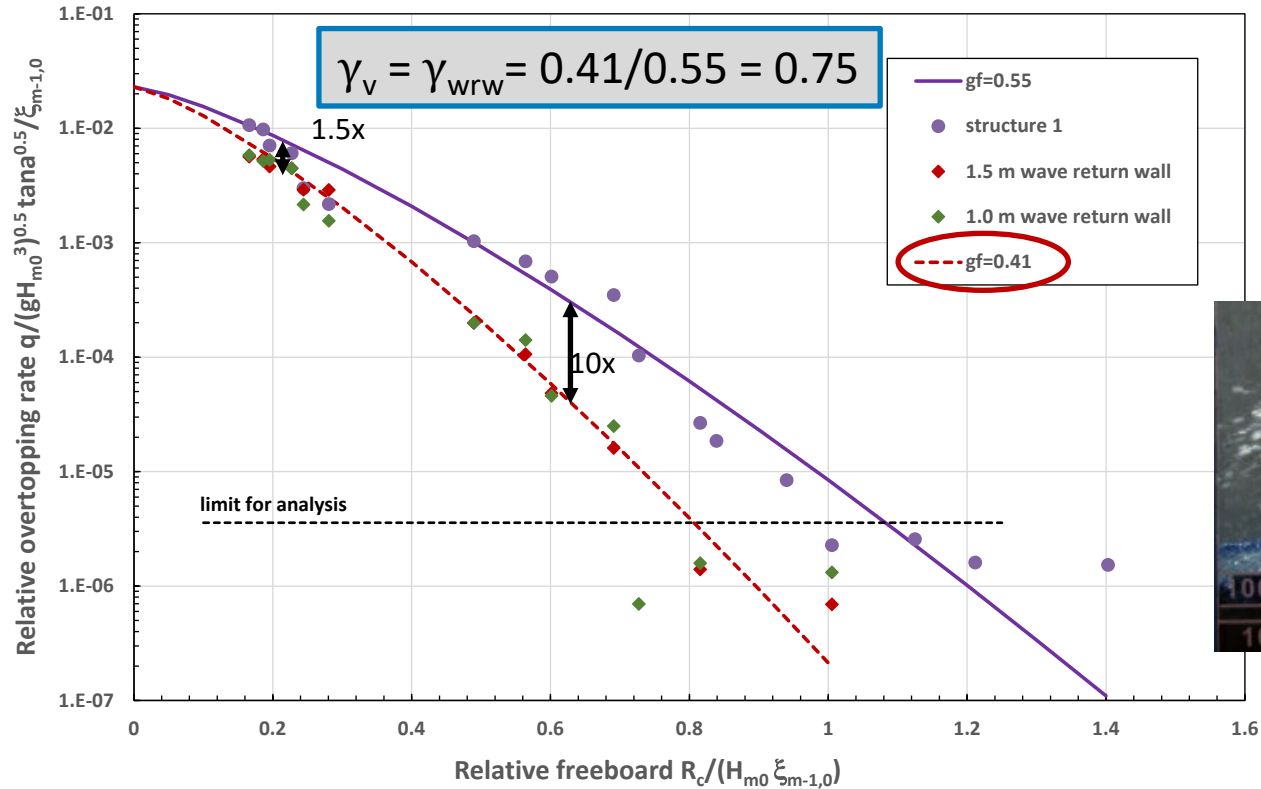
Single pitched; wall and bullnose 1 m



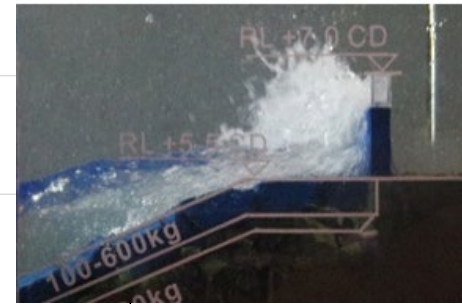
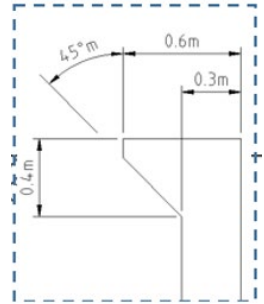
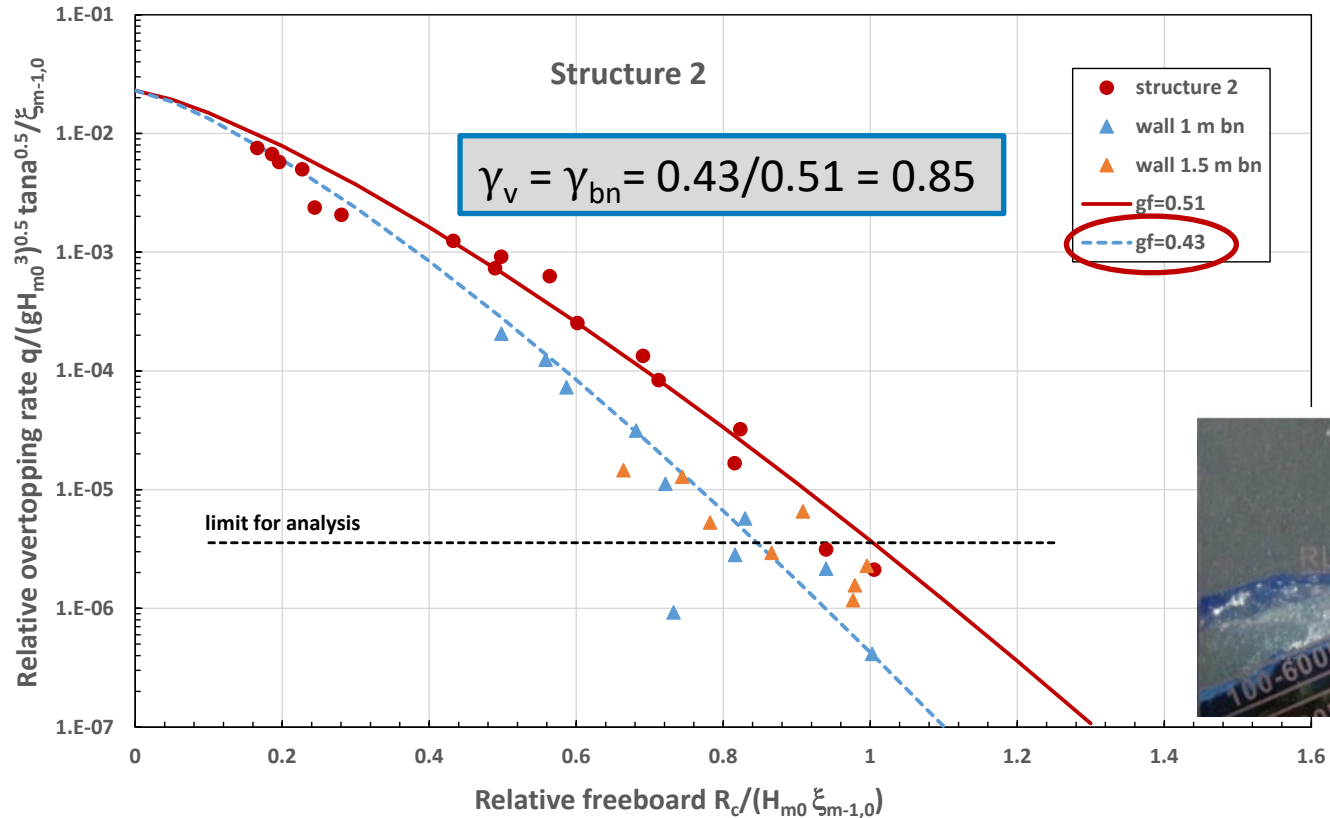
Single pitched; wall and bullnose 1.5 m



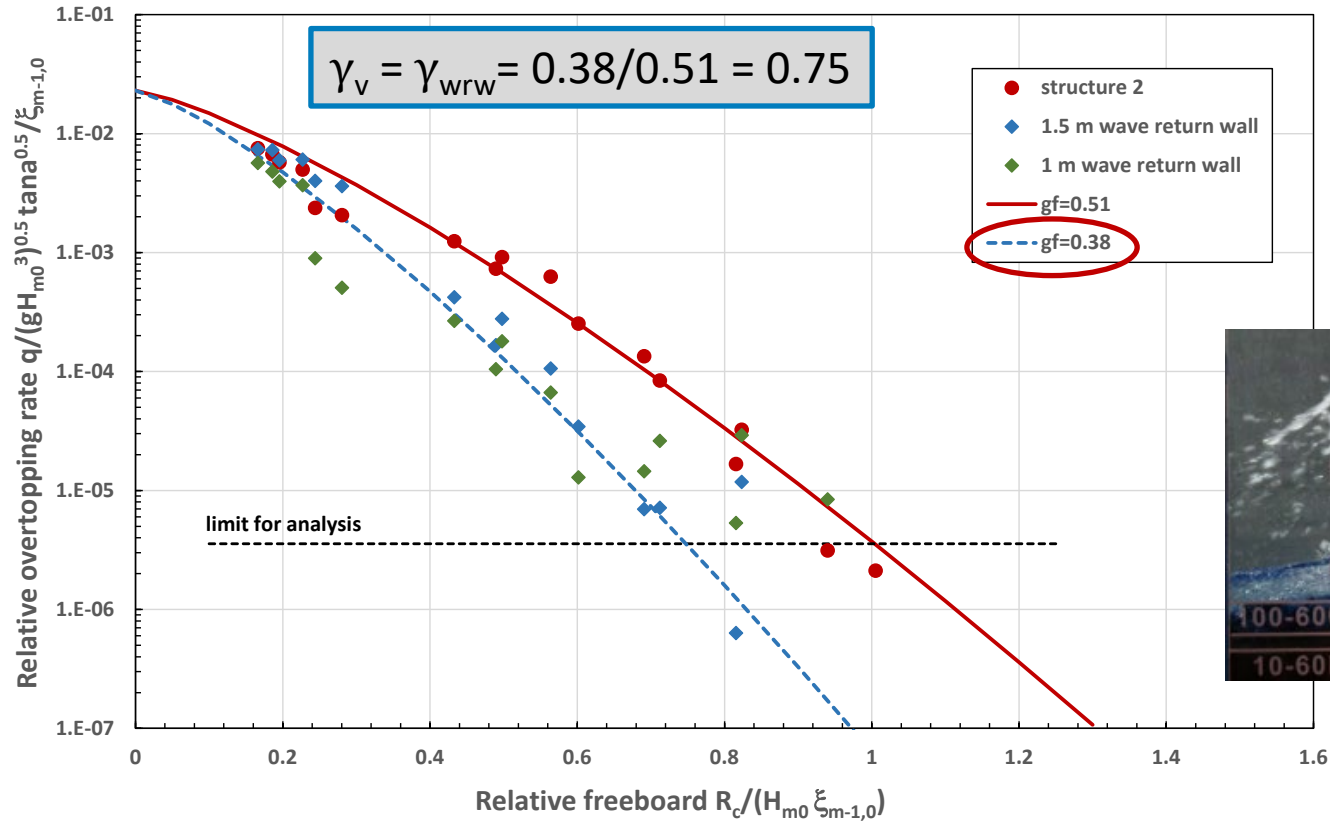
Single pitched; wave return wall



Double pitched; wall 1 m and 1.5 m + bullnose



Double pitched, wave return wall



Conclusions on mitigation options

Restrictions

- (Pitched) rock slopes, one or two layers: mild design wave heights
- Only for high wave steepness: $s_{m-1,0} > 0.035$

Conclusions

- Pitched slopes (above water only) have similar stability as randomly placed rock
- Failure for a single pitched slope occurs at $S_d = 2!$
- Wave wall is very effective, but is an obstacle
- Wave return wall is effective at same crest height
- Model testing gives new influence factors γ_f and γ_v in EurOtop equations

Conclusions on mitigation options

**Vertical walls, with or without bullnose; wave return wall;
a wave steepness $s_{m-1,0} > 0.035$:**

$$\frac{q}{\sqrt{g \cdot H_{m0}^3}} = \frac{0.023}{\sqrt{\tan \alpha}} \gamma_b \cdot \xi_{m-1,0} \cdot \exp\left[-\left(2.7 \frac{R_c}{\xi_{m-1,0} \cdot H_{m0} \cdot \gamma_b \cdot \gamma_f \cdot \gamma_\beta \cdot \gamma_v}\right)^{1.3}\right] \quad \text{EurOtop 5.10}$$

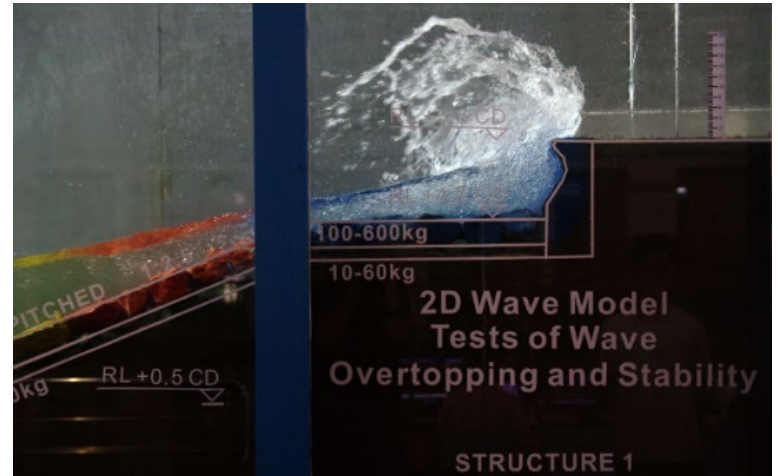
EurOtop random

Single layer of pitched rock:	$\gamma_f = 0.55$	0.6
Double layer of pitched rock:	$\gamma_f = 0.51$	0.55
A vertical wall on top:	$\gamma_v = 1.0$	
A bullnose on the vertical wall:	$\gamma_v = \gamma_{bn} = 0.85$	
A wave return wall	$\gamma_v = \gamma_{wrw} = 0.75$	

Use as max, but do not
apply for surging waves

$$\frac{q}{\sqrt{g \cdot H_{m0}^3}} = 0.09 \cdot \exp\left[-\left(1.5 \frac{R_c}{H_{m0} \cdot \gamma_f \cdot \gamma_\beta \cdot \gamma^*}\right)^{1.3}\right]$$

Thank you



Relationship S_d and N_{od} (Van der Meer, JCHS 2021)

$$S_{d-approx} = 1.32 * N_{od} + 0.95$$

